## Panel Session on Recent Applications of Linear Analysis Techniques

## Some Recent Developments in Small-Signal Stability and Control

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>Several modal analysis applications to power system problems are described, including:

→Hopf bifurcations in the control parameters space

→Modal equivalents of multivariable transfer functions

→Pole - zero analysis in harmonic studies

→Using zeros to understand the adverse terminal voltage transients induced by the presence of PSSs

Compute parameter values that cause crossings of the small-signal stability boundary by critical eigenvalues

> Hopf bifurcations are computed for:

→Single-parameter changes

→Multiple-parameter changes (minimum distance in the parameter space)

## HOPF BIFURCATIONS – TEST SYSTEM UTILIZED

- Brazilian North-South Interconnection: 2,400 buses, 3,400 lines, 120 generators and associated AVRs, 46 stabilizers, 100 speed-governors, 4 SVCs, 2 TCSCs, 1 HVDC link
- Matrix dimension is 13,062 with 48,521 nonzeros and 1,676 states



>Two TCSCs located at each end of the North-South intertie, equiped with PODs to damp the 0.17 Hz mode

The Hopf bifurcation algorithms were applied to compute eigenvalue crossings of the security boundary (5% damping ratio) for gain changes in the two PODs

#### **ROOT CONTOUR WHEN INCREASING THE GAINS OF THE 2 TCSCs**



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>Two crossings of the security boundary were found, both being related to POD gains far away from the nominal values(1 pu):

3.529 > K > 0.108

Computational cost of Hopf bifurcation algorithm

→Single-parameter changes : 0.16 s (per iteration)

→Multiple-parameter changes : 0.35 s (per iteration)

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#### **MODAL EQUIVALENTS OF MULTIVARIABLE TRANSFER FUNCTIONS**

>An m x m transfer function G(s) may be expanded in terms of the system poles and associated residue matrices :

$$\mathbf{G}(s) = \sum_{i=1}^{n} \frac{\mathbf{R}_{i}}{s - \lambda_{i}}$$

>The truncated sum below is the modal equivalent:

$$\mathbf{G}(s) \approx \sum_{i=1}^{p} \frac{\mathbf{R}_{i}}{s - \lambda_{i}}$$
, where  $p \ll n$ 

#### **MODAL EQUIVALENTS OF MULTIVARIABLE TRANSFER FUNCTIONS**

> Sigma-plot for 8 x 8 G(s), ξ = 15%

Full Model has order 1,676 while Modal Equivalent has order 41



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#### **MODAL EQUIVALENTS OF MULTIVARIABLE TRANSFER FUNCTIONS**

Step responses for g<sub>ij</sub>(s) scalar transfer functions for the full model and the 41<sup>st</sup>-order modal equivalent



> Note: Vertical axes given in rad/s and horizontal axes in seconds

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## **Background**

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Harmonic voltage distortions in a system depend on the proximity of its poles and zeros with respect to the characteristic harmonic frequencies

Modal analysis finds poles, zeros and their respective sensitivities to system parameters

>Determines most effective parameter changes in order to reduce harmonic voltage distortion > The Y(s) matrix and its derivative can be rapidly built

>Frequency-dependent components and distributedparameter lines can be efficient and accurately modeled

## Y(s) matrix is always of much lower dimension than state-space or descriptor system models

>Test System



> RLC System Model with Harmonic Current Sources and Capacitors to be Changed



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#### > Resonance frequencies and sensitivities (Fundamental freq.: 50 Hz)

	System poles			Zeros seen from					
				Bus 1		Bus 2		Bus 3	
	1	2	3	1	2	1	2	1	2
f(Hz)	252	489	722	425	565	332	633	382	704
$L_{CC}$	-101	-11	-50	0	0	-48	-80	-88	-47
$L_2$	-3	-4	-2	0	-7	0	0	-5	-2
$L_3$	-4	-2	0	-5	0	-5	-1	0	0
$L_{12}$	-2	-78	-247	0	-290	-40	-66	-37	-289
$L_{13}$	-19	-151	-78	-211	0	-75	-172	-59	-32
$C_{l}$	-45	-12	-206	0	0	-38	-242	-85	-189
$C_2$	-25	-116	-111	0	-269	0	0	-109	-145
$\overline{C_3}$	-54	-114	-28	-210	0	-127	-72	0	0

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- >Newton-Raphson Method Used to Shift Poles and/or Zeros Based on Sensitivities
- > Reductions of 70% and 90% in the impedance magnitudes at 250Hz and at 550Hz were achieved (notably lower harmonic distortions!)



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>Y(s) technology may become a common upgrade to conventional harmonic analysis programs - Y( $j\omega$ )

Efficient eigensolution methods now exist for finding poles of generic Y(s) models

Computationally expensive QR and QZ eigensolution algorithms are no longer needed

## ADVERSE IMPACTS ON TERMINAL VOLTAGE DUE TO PSSS

Studying zeros to understand the adverse voltage transients induced by the presence of PSSs

Comparing the performances of PSSs derived from either rotor speed or terminal power signals

>More detailed presentation on this topic:

→ Power System Stability Controls paper session

→Tuesday, January 29 – 8h00-12h00 / Regent Parlor

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## ACTIVE POWER CHANGES FOLLOWING $\Delta P$ MEC IN SMIB



## **REACTIVE POWER CHANGES FOLLOWING** $\Delta \mathbf{P}$ **MEC IN SMIB**



## POLE-ZERO MAP FOR $\Delta QT / \Delta PMEC (PSSPT)$

#### > Zero near the origin causes bigger overshoot in the step response



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## POLE-ZERO MAP FOR $\Delta QT / \Delta PMEC (PSS\omega)$





# Important developments and increased use of modal analysis

## >Large-scale, control-oriented eigenanalysis

## >Much room for further improvements